

THE MECHANICAL PROPERTIES OF C/C COMPOSITES AS RELATED TO ITS RESISTANCE TO HIGH TEMPERATURE EROSION

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Introduction

Most high temperature aerospace applications of Carbon/Carbon (C/C) composites are implicated by erosion. The implementation of new C/C composites in these systems is often not considered due to the lack of their erosion resistance information. Evaluation of this property needs either field testing, which is very expensive and not always accessible, or a proper simulation. The arc tunnel facility provides combined high temperature / jet stream conditions, in which comparative erosion results are obtained. However this testing is quite expensive as well and hence should be used following a cost effective planning. A better use of the arc tunnel would be to establish a correlation between any of the C/C composites room temperature properties and its resistance to erosion. The present research was planned with this prospective, choosing the mechanical properties as a preliminary selection method of suitable aerospace C/C composites.

Many articles discuss the effects of various types of raw materials and the processing parameters on the mechanical properties of C/C materials [1-3] but only very few deal also with the erosion resistance [4]. No correlation between the composites' mechanical properties and its erosion resistance is reported, though the architecture (weave type, number of directions, volume fraction of fibers) and the processing (final graphitization, number of densifications) effects on the erosion itself are discussed. As for the mechanical properties of the C/C composites, its variations as related to the fibers type and the matrix precursor type are mentioned in few sources. The fiber/matrix bonding and the fibers surface treatment are believed to have a major effect on the flexure and the interlaminar shear results tested in 1D composites [1-3]. The authors claim that the composite with the PAN-based, high tenacity HTA fibers is much weaker than the PAN-based high modulus fibers composite. It is also mentioned that the role of the matrix / fiber bonding is far more important in the carbonized stage, than in the graphitized. However, the major differences in the composites' strength are a result of the heat treatment, rather than the fibers type.

Experimental

Materials

C/C composite specimens from three types, as related to the fibers, were fabricated. All PAN-based fiber type, two high modulus and one high tenacity fibers with various surface treatments. The single filament properties of each fiber are summarized in Table 1. Multidirectional C/C composites were fabricated with each one of these fibers. Six cycles of coal tar pitch impregnation and carbonization under high pressure (HiPIC), followed by about 2600°C graphitizations between each cycle, were used for the densification of a phenolic resin stabilized grid.

Specimens Preparation and Testing

Specimens for mechanical testing were prepared based on standard ASTM methods : ASTM D-638 type 4 or double sized type 5 specimens for tension, ASTM D-695 for compression, ASTM C-651 for testing in 4 points flexure mode [5]. Both the strength and the moduli were evaluated.

Rectangular specimens were prepared for the erosion resistance test in the arc tunnel facility. Measurements during the test included the power supply, the air jet fluxes and pressures, the enthalpy, the backside temperatures at few points and the total time. Measurements before and following the test included weight, size changes at few points, Computed Tomography (CT) nondestructive evaluation and microstructure analysis Scanning Electron Microscopy (SEM and Semquant), on Jeol JSM-84.

Results

The following Table 2 summarizes the densities and the average mechanical properties of the C/C composites specimens. The erosion resistance results in the x and z directions are summarized in Table 3. CT results are given in Table 4.

Discussion and conclusions

Minor differences in the mechanical properties, as well as the erosion resistances are observed with all the three compared C/C composites, though significant differences are reported in the single filament properties of each

fiber. According to these results it seems that, unlike the behavior in polymeric matrix composites, the initial filament properties are less indicative to the C/C composites properties, at least when all the fibers are PAN-based. Even the different surface treatments do not seem to significantly change all the tested properties. A somewhat lower erosion rate is observed in the z direction of the HT reinforced fibers composite, probably as a result of a higher resin-based, glass-like carbon existing in this material, as observed by the initial CT evaluations. CT results following the arc tunnel testing prevail mechanisms of erosion otherwise not detected, i.e. a depletion of material under the surface of the HT fibers composite, while the surface itself is densified, probably due to carbon vapors deposition. The results obtained so far, fail to distinguish between the composites according to the fiber's mechanical properties, hence conclusions couldn't be drawn as to the relationship between them and the erosion resistance. Further research in this direction is planned.

References

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Table 1. The single filament properties of the PAN-based fibers used to reinforce the C/C composites.

| Fiber Type | Tensile Strength MPa | Tensile Modulus GPa | Elongation % | Density gr./cc | Diameter μ m |
|------------|----------------------|---------------------|--------------|----------------|------------------|
| HM A | 3240 | 355 | 0.9 | 1.76 | 7 |
| HM B | 2400 | 343 | 0.9 | 1.8 | 6.7 |
| HT | 3000 | 235 | 1.3 | 1.77 | 7 |

Table 2 : The average mechanical results of 3 types of C/C composites, each containing a different fiber, all identically processed and tested in direction x.

| Fiber Type | C/C Density gr./cc | Tension | Compression | Bending | Tension | Compression | Bending |
|------------|--------------------|--------------|-------------|---------|-------------|-------------|---------|
| | | Strength MPa | | | Modulus GPa | | |
| HM A | 1.942 | 86 | 72 | 92 | 52 | 46 | 60 |
| HM B | 1.965 | 105 | 85 | 110 | 52 | 40 | 52 |
| HT | 1.91 | 108 | 79 | 115 | 48 | 49 | 58 |

Table 3 : The average erosion resistance results of 3 types of C/C composites, tested in x/z direction.

| Direction | Fiber Type | C/C Density gr./cc | Erosion Rate A | Erosion Rate B | Erosion Rate C | Total Wt. Loss % |
|-----------|------------|--------------------|----------------|----------------|----------------|------------------|
| | | | mm/sec | mm/sec | mm/sec | |
| x | HM A | 1.942 | 0.264 | 0.221 | 0.071 | 15.30 |
| x | HM B | 1.965 | 0.233 | 0.225 | 0.086 | 12.70 |
| x | HT | 1.91 | 0.266 | 0.226 | 0.072 | 13.44 |
| z | HM A | 1.942 | 0.283 | 0.220 | 0.080 | 14.52 |
| z | HT | 1.91 | 0.255 | 0.215 | 0.070 | 14.10 |

Table 4 : The CT scanning results of 2 C/C composites following erosion tests.

| Fiber Type | Initial Density | CT based Density* | CT value | | | | |
|------------|-----------------|-------------------|--------------|---------|-----|--------|--------|
| | | | Average | Surface | Top | Center | Bottom |
| HM A | 1.942 | 1.915 | 630 \pm 27 | 754 | 672 | 579 | 626 |
| HT | 1.91 | 1.795 | 557 \pm 29 | | 559 | 515 | 543 |

* The average CT values are translated to density units using a calibration graph.